

Technical Webinar Series 2021

"The I-Gard Difference"



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July 12th, 2021



A client wants to use HRG technology in their next project BUT is not sure whether to purchase from a relay supplier who partners with a resistor company or a resistor supplier who uses someone else's relay or PLC and THEREFORE wants to know if I-Gard is any different.





NGRs Production Area



Relay/Electronics Production Area

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- We make resistors
- We make relays
- We develop new relays
- Everything under one roof
- Integrated solutions







"I-Gard stands behind the design, manufacturing and the functionality of the whole HRG system"



A consultant is looking to include resistor monitoring in the project specification as required by CEC 2021 BUT the resistor in question is rated 2400V 400A and the sensing resistor needs to be able to detect a fault at 6 ohms THEREFORE they are considering the I-Gard SIGMA 3 relay for the project. What makes the SIGMA 3 relay different?



CEC 2021 Table 17

Table 17

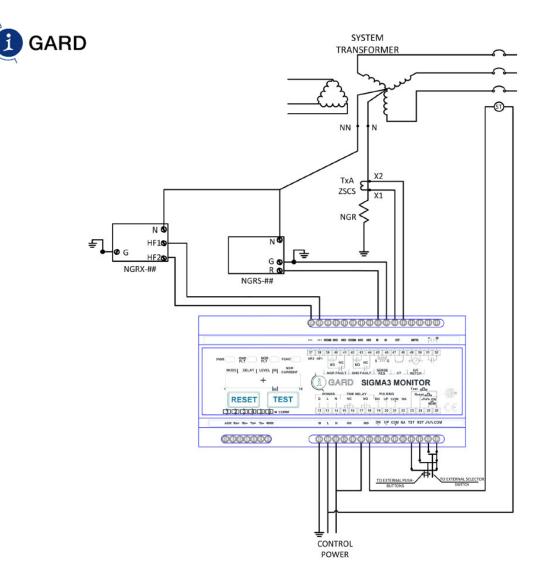
Impedance grounded systems — Conditions for initiation of automatic alarm and de-energization of the system

(See Rule 10-302.)

		Conditions for initiation	of automatic alarm and de	energization of system			
Impedance ground configuration	ed system	Ground fault on current-carrying conductors	Ground fault on conductor from source to impedance grounding device	Loss of continuity from the source through the impedance grounding device to the grounded conductive parts of equipment			
Line-to-neutral loads (4-wire), all voltages/		Alarm and de-energize system immediately	Alarm and de-energize system immediately	Alarm and de-energize system immediately			
Line-to-neutral loads are not served (3-wire) System is • 5 kV or less: and	Scenario 1 [see Note a)]	Alarm and de-energize system within the time rating of the impedance grounding device	Alarm and de-energize system within 48 h	Alarm			
ground fault is limited to 10 A or less	Scenario 2 [see Note b)]	Alarm and de-energize system within the time rating of the impedance grounding device	Alarm and de-energize system within 48 h	Alarm and de-energize system within 48 h			
Line-to-neutral loads are not served (3-wire) System is • greater than	Scenario 1 [see Note a)]	Alarm and de-energize system within the lesser of 48 h or the time rating of the impedance grounding device	Alarm and de-energize system within 48 h	Alarm			
5 kV; or • ground fault is greater than 10 A	Scenario 2 [see Note b)]	Alarm and de-energize system within the lesser of 48 h or the time rating of the impedance grounding device	Alarm and de-energize system within 48 h	Alarm and de-energize system within 48 h			

Note: On the occurrence of a loss of continuity of the impedance grounding circuit from the system source through the impedance grounding device to the grounded non-current-carrying conductive parts of the electrical system, the device monitoring the system can operate in one of two ways:

- it can continue to detect a ground fault on an ungrounded system; or
- it can no longer detect a ground fault on an ungrounded system.





Sigma3

- Ground Fault Relay
- Resistor Monitoring as per CEC 2021

Suitable for:

- LRG systems
- HRG systems



Other relays from competitors

	System Voltage	400	600	690	1000	2400	4200	6000	6600	7200	11000	13800	14400	25000
Current														
1		231 Ω	346.5 Ω	398.4 Ω	577.4 Ω	1385.7 Ω	2424.9 Ω							
5		46.2 Ω	69.3 Ω	79.7 Ω	115.5 Ω	277.2 Ω	485 Ω	692.9 Ω	762.2 Ω	831.4 Ω	1270.2 Ω	1593.5 Ω	1662.8 Ω	
10		23.1 Ω	34.7 Ω	39.9 Ω	57.8 Ω	138.6 Ω	242.5 Ω	346.5 Ω	381.1 Ω	415.7 Ω	635.1 Ω	796.8 Ω	831.4 Ω	1443.4 Ω
15		15.4 Ω	23.1 Ω	26.6 Ω	38.5 Ω	92.4 Ω	161.7 Ω	231 Ω	254.1 Ω	277.2 Ω	423.4 Ω	531.2 Ω	554.3 Ω	962.3 Ω
20			17.4 Ω	20 Ω	28.9 Ω	69.3 Ω	121.3 Ω	173.3 Ω	191 Ω	208 Ω	318 Ω	399 Ω	416 Ω	722 Ω
25				16 Ω	23.1 Ω	55.5 Ω	97 Ω	138.6 Ω	153 Ω	167 Ω	255 Ω	319 Ω	333 Ω	578 Ω
30					19.3 Ω	46.2 Ω	80.9 Ω	115.5 Ω	128 Ω	139 Ω	212 Ω	266 Ω	278 Ω	482 Ω
40						34.7 Ω	60.7 Ω	86.7 Ω	96 Ω	104 Ω	159 Ω	200 Ω	208 Ω	361 Ω
50						27.8 Ω	48.5 Ω		77 Ω	84 Ω	128 Ω	160 Ω	167 Ω	289 Ω
100							24.3 Ω			42 Ω		80 Ω	84 Ω	145 Ω
200														
300														
400														

** Values highlighted in yellow

Limited temperature Range 0-40°C



I-Gard Monitoring

Sys	System Voltage		600	690	1000	2400	4200	6000	6600	7200	11000	13800	14400	25000
Current														
1		231 Ω	346.5 Ω	398.4 Ω	577.4 Ω	1385.7 Ω	2424.9 Ω							
5	5	46.2 Ω	69.3 Ω	79.7 Ω	115.5 Ω	277.2 Ω	485 Ω	692.9 Ω	762.2 Ω					
10		23.1 Ω	34.7 Ω	39.9 Ω	57.8 Ω	138.6 Ω	242.5 Ω	346.5 Ω	381.1 Ω	415.7 Ω	635.1 Ω	796.8 Ω	831.4 Ω	1443.4 Ω
15	j	15.4 Ω	23.1 Ω	26.6 Ω	38.5 Ω	92.4 Ω	161.7 Ω	231 Ω	254.1 Ω	277.2 Ω	423.4 Ω	531.2 Ω	554.3 Ω	962.3 Ω
20		11.6 Ω	17.4 Ω	20 Ω	28.9 Ω	69.3 Ω	121.3 Ω	173.3 Ω	190.6 Ω	207.9 Ω	317.6 Ω	398.4 Ω	415.7 Ω	721.7 Ω
25		9.3 Ω	13.9 Ω	16 Ω	23.1 Ω	55.5 Ω	97 Ω	138.6 Ω	152.5 Ω	166.3 Ω	254.1 Ω	318.7 Ω	332.6 Ω	577.4 Ω
30		7.7 Ω	11.6 Ω	13.3 Ω	19.3 Ω	46.2 Ω	80.9 Ω	115.5 Ω	127.1 Ω	138.6 Ω	211.7 Ω	265.6 Ω	277.2 Ω	481.2 Ω
40		5.8 Ω	8.7 Ω	10 Ω	14.5 Ω	34.7 Ω	60.7 Ω	86.7 Ω	95.3 Ω	104 Ω	158.8 Ω	199.2 Ω	207.9 Ω	360.9 Ω
50			7 Ω	8 Ω	11.6 Ω	27.8 Ω	48.5 Ω	69.3 Ω	76.3 Ω	83.2 Ω	127.1 Ω	159.4 Ω	166.3 Ω	288.7 Ω
100)				5.8 Ω	13.9 Ω	24.3 Ω	34.7 Ω	38.2 Ω	41.6 Ω	63.6 Ω	79.7 Ω	83.2 Ω	144.4 Ω
200						7 Ω	12.2 Ω	17.4 Ω	19.1 Ω	20.8 Ω	31.8 Ω	39.9 Ω	41.6 Ω	72.2 Ω
300							8.1 Ω	11.6 Ω	12.8 Ω	13.9 Ω	21.2 Ω	26.6 Ω	27.8 Ω	48.2 Ω
400							6.1 Ω	8.7 Ω	9.6 Ω	10.4 Ω	15.9 Ω	20 Ω	20.8 Ω	36.1 Ω
800											8 Ω	10 Ω	10.4 Ω	18.1 Ω

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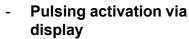
I-Gard vs competitors

		400		500		690	1	.000		2400		4200		5000		600		7200	1:	1000	1	3800	1	4400	2	5000
	I-GARD	Comp	I-GARD	Comp	I-GARD	Comp	I-GARD	Comp	I-GARD	Comp	I-GARD	Comp	I-GARD	Comp	I-GARD	Comp	I-GARD	Comp	I-GARD	Comp	I-GARD	Comp	I-GARD	Comp	I-GARD	Comp
Current																										
	1231 Ω	231 Ω	346.5 Ω	346.5 Ω	398.4 Ω	398.4 Ω	577.4 Ω	577.4 Ω	1385.7	<mark>Ω</mark> 1385.7	2424.9	<mark>Ω</mark> 2424.9 Ω	2				_									
!	46.2 Ω	46.2 Ω	69.3 Ω	69.3 Ω	79.7 Ω	79.7 Ω	115.5 Ω	115.5 Ω	277.2	277.2 Ω	485 Ω	485 Ω	692.9 C	692.9 Ω	762.2 Ω	762.2 Ω		831.4 Ω		1270.2	2	1593.5 Ω				
10	23.1 Ω	23.1 Ω	34.7 Ω	34.7 Ω	39.9 Ω	39.9 Ω	57.8 Ω	57.8 Ω	138.6 C	138.6 Ω	242.5 C	242.5 Ω	346.5 C	346.5 Ω	381.1 C	381.1 Ω	415.7 Ω	415.7 Ω	635.1 Ω	635.1 Ω	796.8 Ω	796.8 Ω	1443.4	1443.4 Ω	1443.4 C	1443.4
1	15.4 Ω	15.4 Ω	23.1 Ω	23.1 Ω	26.6 Ω	26.6 Ω	38.5 Ω	38.5 Ω	92.4 Ω	92.4 Ω	161.7 C	161.7 Ω	231 Ω	231 Ω	254.1 C	254.1 Ω	277.2 Ω	277.2 Ω	423.4 Ω	423.4 Ω	531.2 Ω	531.2 Ω	962.3 Ω	962.3 Ω	962.3 Ω	962.3 Ω
2	11.6 Ω		17.4 Ω	17.4 Ω	20 Ω	20 Ω	28.9 Ω	28.9 Ω	69.3 Ω	69.3 Ω	121.3 C	121.3 Ω	173.3 C	173.3 Ω	190.6 ຕ	191 Ω	207.9 Ω	208 Ω	317.6 Ω	318 Ω	398.4 Ω	399 Ω	721.7 Ω	722 Ω	721.7 Ω	722 Ω
2	9.3 Ω		13.9 Ω		16 Ω	16 Ω	23.1 Ω	23.1 Ω	55.5 Ω	55.5 Ω	97 Ω	97 Ω	138.6	138.6 Ω	152.5 Ω	153 Ω	166.3 Ω	167 Ω	254.1 Ω	255 Ω	318.7 Ω	319 Ω	577.4 Ω	578 Ω	577.4 Ω	578 Ω
3	7.7 Ω		11.6 Ω		13.3 Ω		19.3 Ω	19.3 Ω	46.2 Ω	46.2 Ω	80.9 Ω	80.9 Ω	115.5 C	115.5 Ω	127.1 C	128 Ω	138.6 Ω	139 Ω	211.7 Ω	212 Ω	265.6 Ω	266 Ω	481.2 Ω	482 Ω	481.2 Ω	482 Ω
4	5.8 Ω		8.7 Ω		10 Ω		14.5 Ω		34.7 Ω	34.7 Ω	60.7 Ω	60.7 Ω	86.7 Ω	86.7 Ω	95.3 Ω	96 Ω	104 Ω	104 Ω	158.8 Ω	159 Ω	199.2 Ω	200 Ω	360.9 Ω	361 Ω	360.9 Ω	361 Ω
5)		7 Ω		8 Ω		11.6 Ω		27.8 Ω	27.8 Ω	48.5 Ω	48.5 Ω	69.3 Ω		76.3 Ω	77 Ω	83.2 Ω	84 Ω	127.1 Ω	128 Ω	159.4 Ω	160 Ω	288.7 Ω	289 Ω	288.7 Ω	289 Ω
10)						5.8 Ω		13.9 Ω		24.3 Ω	24.3 Ω	34.7 Ω		38.2 Ω		41.6 Ω	42 Ω	63.6 Ω		79.7 Ω	80 Ω	144.4 Ω	145 Ω	144.4 Ω	145 Ω
20)								7 Ω		12.2 Ω		17.4 Ω		19.1 Ω		20.8 Ω		31.8 Ω		39.9 Ω		72.2 Ω		72.2 Ω	
30	D										8.1 Ω		11.6 Ω		12.8 Ω		13.9 Ω		21.2 Ω		26.6 Ω		48.2 Ω		48.2 Ω	
40)										6.1 Ω		8.7 Ω		9.6 Ω		10.4 Ω		15.9 Ω		20 Ω		36.1 Ω		36.1 Ω	
80)																		8 Ω		10 Ω		18.1 Ω			



I-Gard Sigma3 - TDM Touchscreen Display







- Control and calibration
- Event recording





- Communication Settings
- Modbus RTU
- Modbus TCP/IP



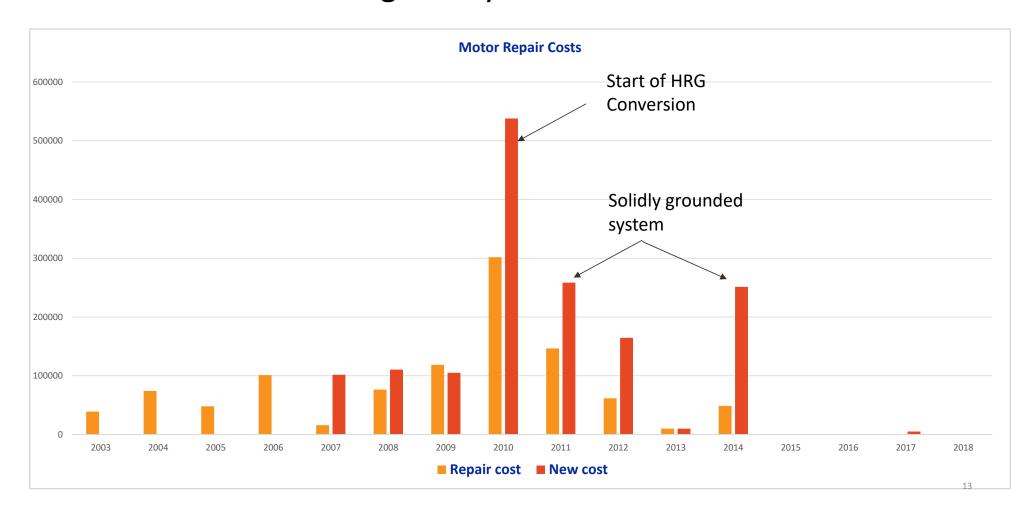




Facility operator has a solidly grounded system since this system trips when there is a ground fault BUT the trip level is so high that motors are being damaged and THEREFORE they are considering switching to High Resistance Grounded. What is the major difference with respect to motor damage between these two grounding systems?



Pulp and Paper Mill case Converting Solidly Grounded to HRG

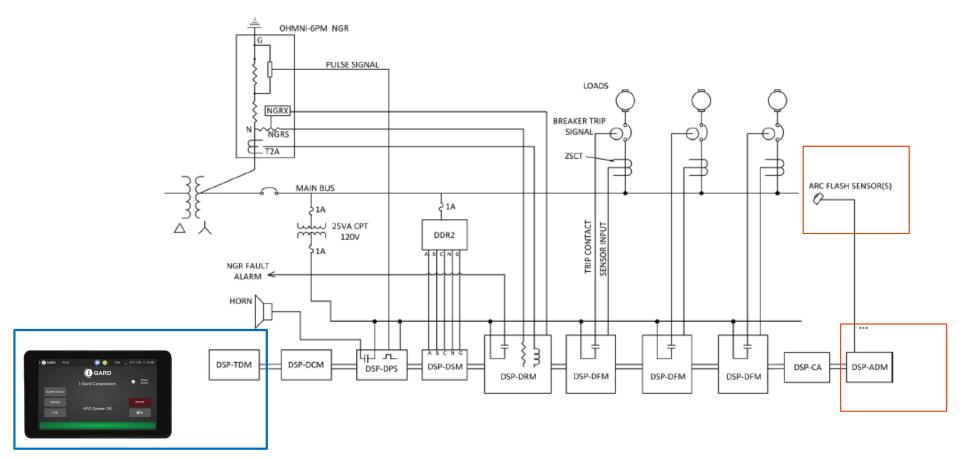




A long term proponent of HRG technology was pushing for their facility to be upgraded BUT the decision maker was concerned that HRG reduces the probability of an arc flash BUT not the incident energy levels THEREFORE the proposal is to consider Advanced HRG. What makes Advanced HRG different from standard HRG with respect to incident energy levels?



I-Gard DSP- System Advanced HRG system





NFPA70E Annex O Advanced HRG system

O.2.2 Design option decisions should facilitate the ability to eliminate hazards or reduce risk by doing the following:

- 1. Reducing the likelihood of exposure, and
- 2. Reducing the magnitude of exposure
- 3. Enabling achievement of an electrically safe work condition

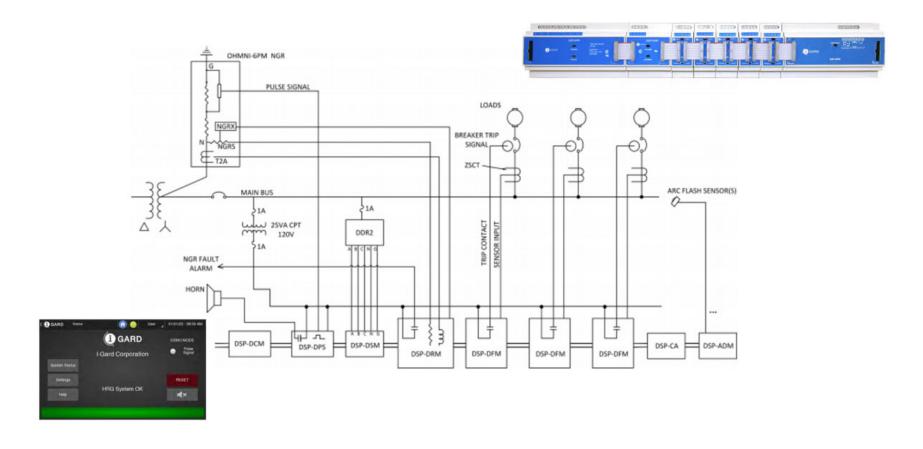
"I-Gard's Advanced HRG system (DSP-OHMNI relay) is the only in the market that reduces the likelihood and the severity of any arc flash event. All in one single relay"



The maintenance manager at a large petrochemical facility valued the process continuity aspect of using HRG BUT was concerned that maintenance personnel would not look for the fault in a timely manner THEREFORE she wanted to consider Advanced HRG?

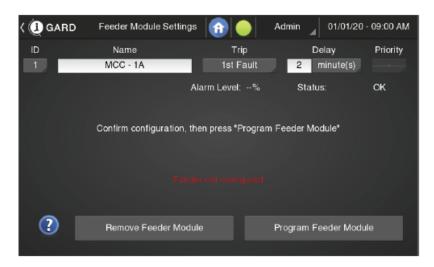


I-Gard DSP- System (Advanced HRG system)





Standard HRG vs Advanced HRG



Trip on 1st fault with delay



Trip on 2nd fault & Priority Level



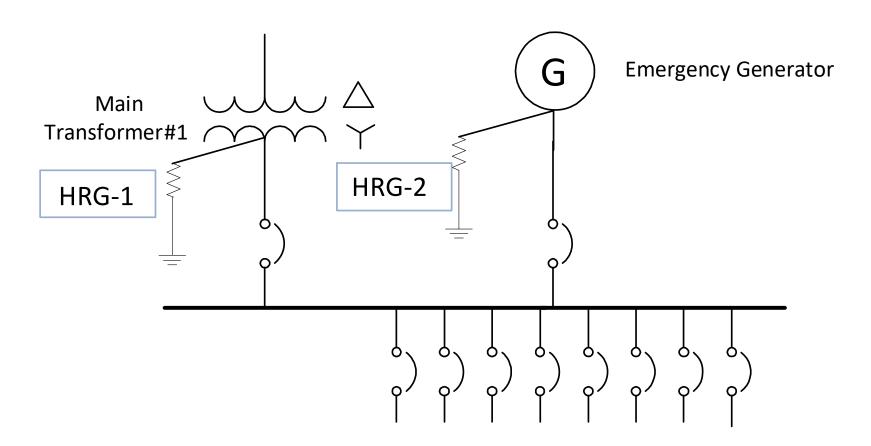
19



A consultant is considering HRG for a data center BUT is unclear whether there is a need for two HRG systems, one on the transformer and one on the generator THEREFORE is considering asking I-Gard for application support. Is there anything different about the I-Gard approach to this application?

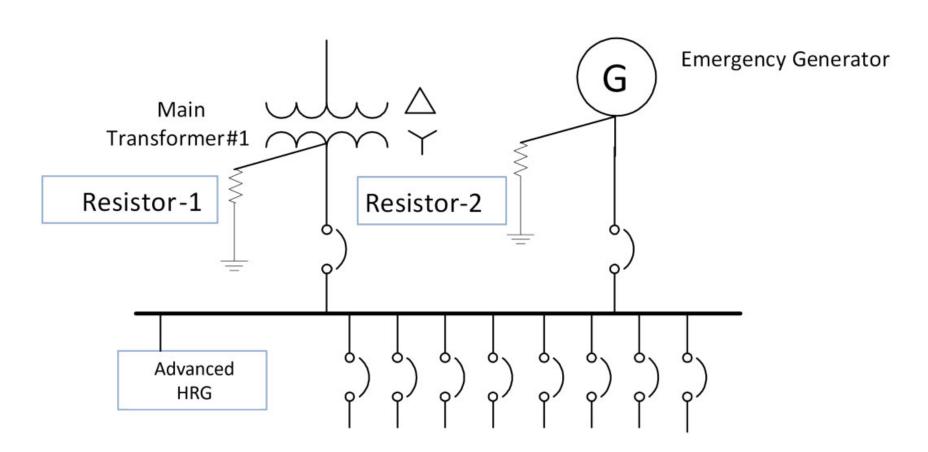


Typical Datacenter Topology





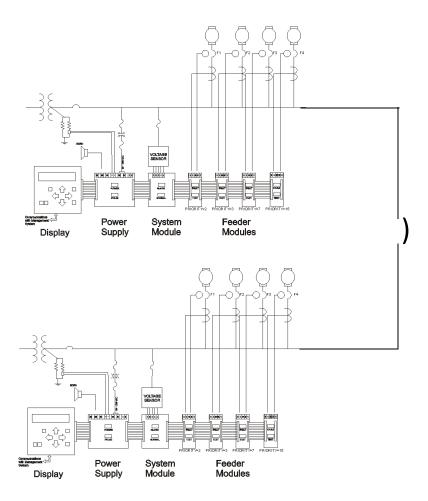
New Datacenter Topology



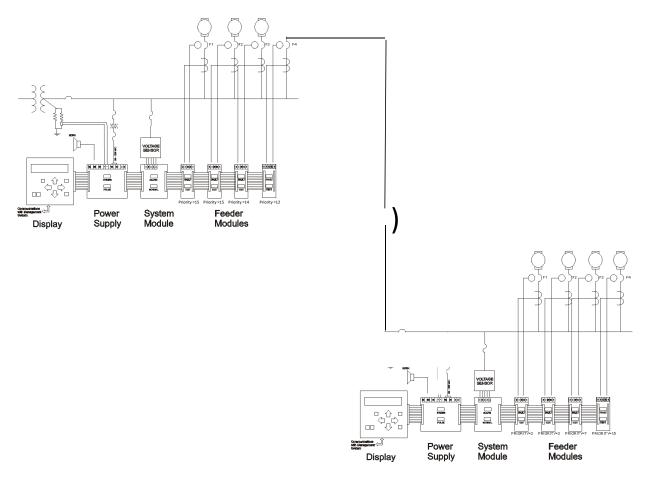


A mining company has used standard HRG in the past BUT is looking to upgrade to feeder protection THEREFORE needs to understand what are the limits on number of feeders and tripping time.





(I) GARD



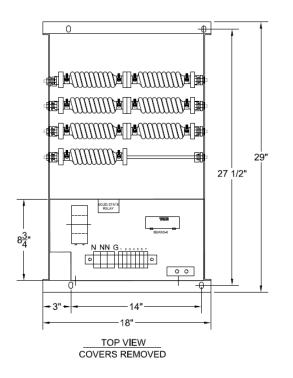


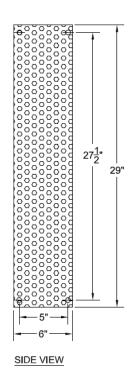
An OEM is looking to integrate HRG technology BUT space is a limitation and THEREFORE need the smallest possible footprint. What makes the I-Gard HRG different?



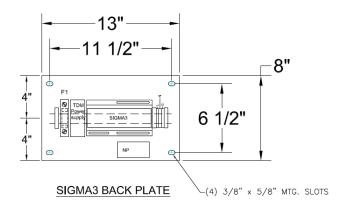
I-Gard High Resistance Grounding HRG-OEM Kit

(1. Resistor)





(2. Sigma3 back plate)







I-Gard HRG Systems

HRG- OEM kit

(3. Sigma3-TDM)



- 1. Resistor
- 2. Sigma3 back plate
- 3. Sigma3-TDM Touchscreen Display Module

Wall mounted HRG



Sleuth with Pulsing Capability & Sigma3 - TDM



A consultant is specifying a NGR and typically references IEEE C57.32 BUT the project is in Canada and THEREFORE the reference standard will be CSA 22.2-295, what is the difference between the standards?



Standards in Use

•	IEEE 32-1972 (R 1990)	"IEEE Standard Requirements, Terminology, and Test Procedures for Neutral Grounding Devices"
•	IEEE C57.32-2015	"IEEE Standard for Requirements, Terminology, and Test Procedures for Neutral Grounding Devices"
•	IEEE C57.32a-2020	"IEEE Standard for Requirements, Terminology, and Test Procedures for Neutral Grounding Devices"

"Neutral grounding devices"

• **IEC 60076 25** In Process

• CSA C22.2 No. 295-15



Terminology

- Rated Voltage
- Rated Current
- Rated Time
- Maximum Temperature
- Temperature Coefficient of Resistance



Rated Voltage

Since the active material used in resistors has an appreciable temperature coefficient, the resistance is materially changed during the time of operation causing the current to decrease. When the product of the fault current and resistance at 30 °C exceeds 80% of the line-to-neutral voltage of the circuit, the resistor shall be rated for constant voltage and the rated voltage shall be taken equal to the line-to-neutral voltage.



Rated Current

• The initial current through the resistor.



Rated Time

- Rated time shall be 10 seconds, 1 minute, 10 minutes, extended time, or continuous(steady-state).
- Extended time shall not exceed an average of 90 days per year.



10 s and 1 min. ratings

• The rated-time temperature rise of 10-second and 1-minute devices shall be taken as the sum of the steady-state rise and the additional rise caused by the application of rated voltage for rated time.



Ten-Minute Ratings

• The rated-time temperature rise of 10-minute devices shall be taken as the sum of the steady-state rise, if specified, otherwise 0°C rise if not specified, and the additional rise caused by the application of rated voltage for rated time.



Maximum Temperature Rise

Temperature Rise K				
		IEEE	CSA	IEC
Steady State for continuous current ratings	Steady state (hot-spot)	385	375	385
Rated Time for thermal current	Extended-time (<u>hot-spot</u>)	610	600	610
ratings less than Steady-State	Ten-minute (<u>hot-spot</u>)	610	600	610
	Less than 10 min (<u>hot-spot</u>)	760	750	760



Temperature Coefficient of Resistance

$$\alpha = \frac{R_2 - R_1}{R_1(\theta_2 - \theta_1)} \qquad \qquad R_2 = R_1 \left[1 + \alpha \left(\theta_2 - \theta_1 \right) \right]$$

• Where;

- $-R_1$ is the initial resistance(Ω)
- $-R_2$ is the final resistance(Ω)
- $-\theta_1$ is the Initial Temperature (°C)
- $-\theta_2$ is the final Temperature(°C)
- $-\alpha$ is the Temperature coefficient of resistance(1/ °C)



Mill Test Certificate – Resistors



Electrical resistivity	Type 1	Туре 2	Туре 4
ohm-cir mil/ft at 88°F	720	680	656
microhm-cm at 20°C	120	113	109

Mean Temperature Coefficient of Electrical Resistivity

Tempe	rature	Coeffic	elent
68°F to	20°C to	per °F	per °C
200	93	880000.0	0.000101
400	204	0.000070	0.000126
600	316	0.000085	0.000153
800	427	0.000091	0.000164
1000	538	0.000104	0.000187
1200	649	0.000121	0.000218
1400	760	0.000134	0.000241



Example 1

277 V, 5 A, Continuous resistor.

Rated Voltage= 277 V

Rated Current = 5 A

Rated Time = Continuous

Max Temperature Rise = 385°C

Temperature Coefficient of Resistance = Not Specified

Resistance Change

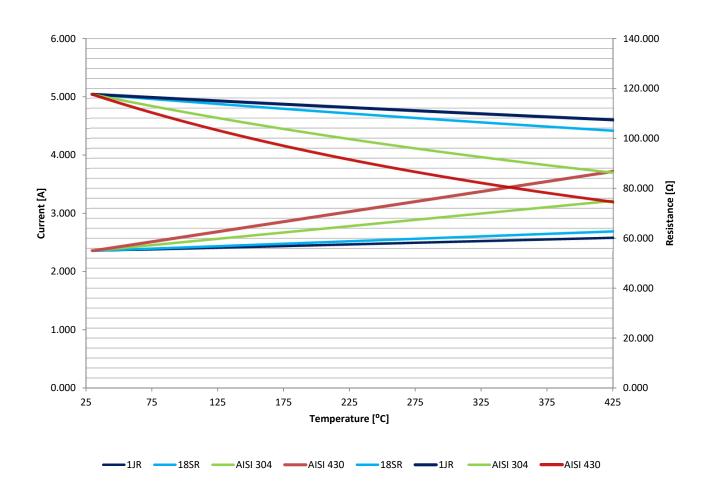
$$S5.4 \, \Omega \qquad 385 \, ^{\circ}\mathrm{C}$$

$$R_2 = R_1 \Big[1 + \alpha \Big(\theta_2 - \theta_1 \Big) \Big]$$

Alloy	Temperature Coefficient of Resistance (1/°C) α	Percent change in Resistance	Current decrease as a percentage
AISI 304	0.00092	35% Increase to 74.79Ω	26.15% to 3.7 A
AISI 430	0.00146	56 % Increase to 86.42 Ω	36% to 3.2 A
18SR	0.000358	13.7 % Increase to 62.989 Ω	12% to 4.39 A
1JR	0.000241	9 % Increase to 60.39Ω	9.1 % to 4.6 A

^{**} First 2 rows violate CSA Standard as the current decreases by more than 20% but no IEEE standard.







Example 2

2400 V, 400 A, 10 seconds resistor.

Rated Voltage= 2400 V

Rated Current = 400 A, continuous portion not specified

Rated Time = 10 s.

Max Temperature Rise = 760°C

Temperature Coefficient of Resistance = Not Specified



Resistance change

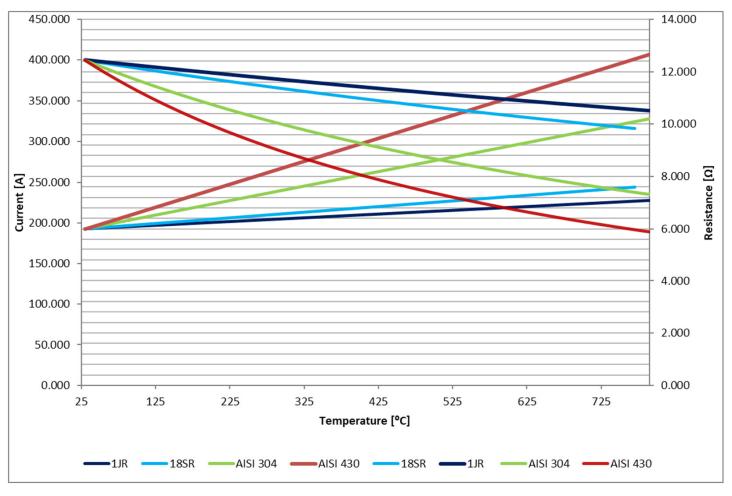
$$R_2 = R_1 \left[1 + \alpha \left(\theta_2 - \theta_1 \right) \right]$$

Alloy	Temperature Coefficient of Resistance (1/°C) α	Percent change in Resistance	Current decrease as a percentage
AISI 304	0.00092	70% Increase to 10.2Ω	41.1% to 235 A
AISI 430	0.00146	110 % Increase to 12.65 Ω	52.5% to 189 A
18SR	0.000358	27 % Increase to 7.63Ω	21% to 314 A
1JR	0.000241	18 % Increase to 7.1Ω	15.4 % to 338 A

^{**} First 3 rows violate ${f CSA}$ Standard as the current decreases by more than 20%

^{**} First 2 rows violate **IEEE C57.32** as resistance increases by more than 67%







<u>Case 10</u>

A customer is looking to conduct absence of voltage testing BUT their current product isn't labeled to UL 1436 which is required by NFPA 70E 120.5 THEREFORE they are looking at the I-Gard i-AVT.



Exception No. 1 to 7:

An adequately rated permanently mounted **absence of voltage tester** shall be permitted to be used to test for the absence of voltage of the conductors or circuit parts at the work location, provided it meets all of the following requirements:

NFPA 70E 2021-120.5 (7) Exception 1.	POWER		
Description	Voltage Indicator	Voltage Test Station	Absence of Voltage Tester
(1) It is permanently mounted and installed in accordance with the manufacturer's instructions	YES	YES	YES
(1) and tests the conductors and circuit parts at the point of work;	NO Test Function	NO - hand held tester is in contact with the test port, no verification that test port is in contact with circuit.	YES
(2) It is listed and labeled for the purpose of testing for the Absence of Voltage	NO	NO	YES
(3) It tests each phase conductor or circuit part both phase-to-phase and phase-to-ground	Only Phase to Ground	YES - with hand held tester	YES
(4) The test device is verified as operating satisfactorily on any known voltage source before and after testing for the Absence of Voltage	NO	NO - no means to verify the test port, the hand held meter requires access to a known voltage source	YES
Note 1: Meets rating and desgin requirements for absence of voltage testers described in UL 1436	NO	NO	YES





	I-Gard	Grace Technologies
	Absence of Voltage Tester	Voltage Test Station
	i-AVT	P-S10S
	13 13 13 13 13 13 13 13 13 13 13 13 13 1	
UL 1436 Requirements		
A permanently-mounted test device that is used to verify that a circuit is de-energized prior to opening an electrical enclosure that contains energized electrical conductors or circuit paths	YES	YES
12.1.2 - An AVT shall be provided with the means for the user to initiate the test for absence of voltage.	YES	NO
12.1.3 - An AVT shall provide the user with a visual indicator to confirm the absence of voltage after the absence of voltage test has been performed. The visual indication shall be green.	YES	NO
12.1.5 - The AVT shall incorporate a supervisory test circuit to verify that the tester is functioning properly before and after the AVT performs voltage measurements.	YES	NO
12.1.4 - The AVT supervisory circuit has incorporated a secondary power source and shall have no internal failure that would affect performance.	YES, SUPER CAPACITOR	NO
12.1.6 - The AVT visual indicator shall only illuminate green when all phase-to-phase and phase-to-ground voltages measure less than 3VAC or 3VDC.	YES	NO
12.1.7 The AVT visual indicators shall not illuminate green unless the phase and ground leads are in direct contact with the circuit conductors being tested	Yes, product architecture and operation ensures green lights can only illuminate once continuity check is complete.	No means of verifying that leads are connected.
12.1.8 - The AVT visual indicator shall not illuminate green if a phase lead is connected to ground or the ground lead is connected to a phase conductor.	Yes, product architecture and operation ensures green lights cannot illuminate if any lead is misconnected	No means of verifying that leads are properly connected
12.1.9 12.1.9 The visual indicator shall not illuminate green unless the secondary power source is operational	Yes, product architecture and operation ensures green lights can only illuminate if the secondary power source is operational	No secondary power source available
12.2.1 - The AVT shall comply with the Standard for Functional Safety IEC 61508 and achieve a SIL 3 rating.	Yes, product is tested and approved to SIL3 safety rating	No the voltage test port is not tested to SIL 3 rating and failsafe in operation



What makes I-Gard i-AVT different?





 The i-AVT provides visual indication of the presence of voltage via 3 phase voltage red lights connected directly to the circuit conductors, thereby indicating that hazardous voltage is present.





 The i-AVT provides positive indication of the Absence of Voltage via 3 Green LED lights.



- The i-AVT provides a continuity check to ensure that all leads are connected and connected properly.
- The i-AVT is maintenance free with secondary power source built-in to the control module.
- The i-AVT is SIL-3 rated ensuring that it will not provide a false positive.



I-Gard VTi





I-Gard VTi







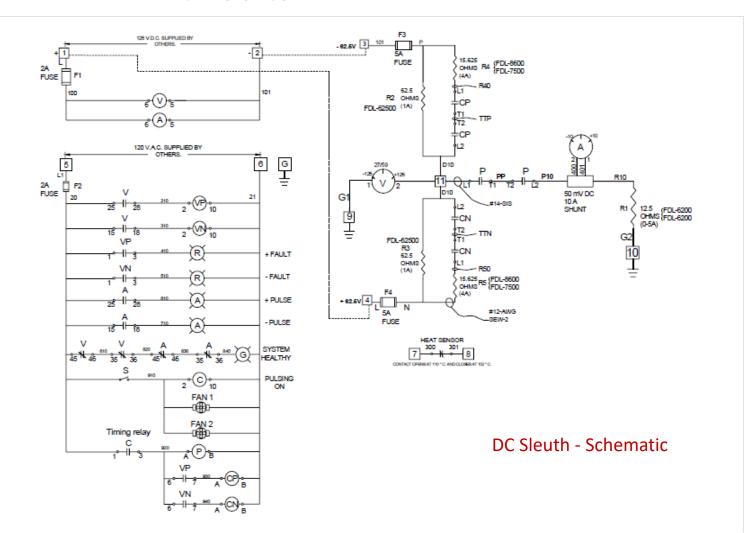
Case 11

A chemical processing facility is upgrading from ungrounded to high resistance grounded BUT has multiple variable frequency drives and is concerned about DC faults THEREFORE needs a solution that detects both AC and DC faults.

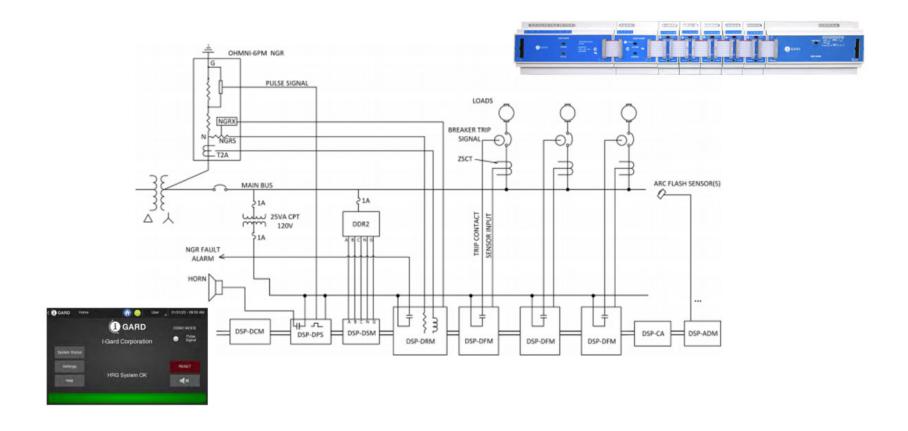


DC Faults

 I-Gard was the first company to produce a DC HRG system.





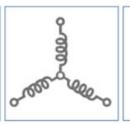


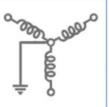


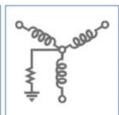
Questions?















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